

This Page Is Inserted by IFW Operations  
and is not a part of the Official Record

## **BEST AVAILABLE IMAGES**

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images may include (but are not limited to):

- BLACK BORDERS
- TEXT CUT OFF AT TOP, BOTTOM OR SIDES
- FADED TEXT
- ILLEGIBLE TEXT
- SKEWED/SLANTED IMAGES
- COLORED PHOTOS
- BLACK OR VERY BLACK AND WHITE DARK PHOTOS
- GRAY SCALE DOCUMENTS

**IMAGES ARE BEST AVAILABLE COPY.**

**As rescanning documents *will not* correct images,  
please do not report the images to the  
Image Problem Mailbox.**

PATENT CLAIMS

1. An electro-optical voltage sensor for measurement of an electrical voltage  $V$ , the voltage  $V$  being present  
5 between two electrodes (3, 4) and generating an electric field, the electrodes (3, 4) being arranged in a manner spaced apart from one another, and an electro-optically active medium (1) being arranged between the electrodes (3, 4), into which medium light (5) can be  
10 radiated, it being possible to influence the state of polarization of said light in the electro-optically active medium (1) by means of the electric field and to detect it after emergence from the electro-optically active medium (1), it being possible to determine the  
15 voltage  $V$  from the detected state of polarization, characterized in that  
a distance medium (2) is arranged between the two  
electrodes (3, 4), the electro-optically active medium (1) being arranged with an effective thickness  $d_1$  and  
20 the distance medium (2) with an effective thickness  $d_2$  between the two electrodes (3, 4) and the effective thicknesses  $d_1$ ,  $d_2$  being chosen in such a way that temperature influences on the detected state of  
polarization of the light (5) are essentially  
25 compensated for.

2. The voltage sensor as claimed in claim 1, characterized in that the effective thickness  $d_2$  of the distance medium (2) and the effective thickness  $d_1$  of  
30 the electro-optically active medium (1) are chosen in such a way that the influences of the temperature dependences of temperature-dependent material constants of the distance medium (2) and of the electro-optically active medium (1) on the detected state of polarization  
35 of the light (5) are essentially compensated for.

3. The voltage sensor as claimed in claim 2, characterized in that the temperature-dependent material constants are

- critical electro-optical coefficients ( $k$ ),
- 5 - dielectric constants ( $\epsilon$ ) and
- thermal expansion coefficients ( $\alpha$ ).

4. The voltage sensor as claimed in claim 1 or 2, characterized in that the effective thickness  $d_2$  of the distance medium (2) and the effective thickness  $d_1$  of the electro-optically active medium (1) are chosen in such a way that the influences of the temperature dependences of the dielectric constant  $\epsilon_1$  of the electro-optically active medium (1) of the dielectric constant  $\epsilon_2$  of the distance medium (2) and,

- if the distance medium (2) is not electro-optically active or the light (5) does not radiate through the distance medium (2): of the critical electro-optical coefficient  $k_1$  of the electro-optically active medium (1), and
- 20 - if both the electro-optically active medium (1) and the distance medium (2) are electro-optically active and light (5) is radiated through them: of the critical electro-optical coefficient  $k_1$  of the electro-optically active medium (1) and of the critical electro-optical coefficient  $k_2$  of the distance medium (2),

on the detected state of polarization of the light (5) essentially cancel one another out.

30

5. The voltage sensor as claimed in claim 4, characterized in that the following holds true:

$$d_1 \cdot [(\partial k_1 / \partial T) \cdot E_1 + k_1 \cdot (\partial E_1 / \partial T)] + d_2 \cdot [(\partial k_2 / \partial T) \cdot E_2 + k_2 \cdot (\partial E_2 / \partial T)] \approx 0$$

if the light (5) also radiates through the distance medium (2), and:

35

$$(\partial k_1 / \partial T) \cdot E_1 + k_1 \cdot (\partial E_1 / \partial T) \approx 0$$

if the light (5) does not radiate through the distance medium (2) or the latter is not electro-optically active;

where  $E_1$  is the electric field strength in the electro-optically active medium (1) and  $E_2$  is the electric field strength in the distance medium (1),  
and in particular where the aforementioned electric field strengths are approximated as

$$E_1 \approx \epsilon_2 \cdot V / (\epsilon_2 \cdot d_1 + \epsilon_1 \cdot d_2) \text{ and}$$
$$E_2 \approx \epsilon_1 \cdot V / (\epsilon_2 \cdot d_1 + \epsilon_1 \cdot d_2)$$

6. The voltage sensor as claimed in one of the preceding claims, characterized in that the distance medium (2) is transparent and of a solid state of aggregation, and in that the light radiates through both the distance medium (2) and the electro-optically active medium (1).

7. The voltage sensor as claimed in one of the preceding claims, characterized in that the distance medium (2) has a vanishing critical electro-optical coefficient  $k_2$  and/or a vanishing temperature dependence  $\partial k_2 / \partial T$  of its critical electro-optical coefficient  $k_2$ , and in particular has a negligible temperature dependence  $\partial \epsilon_2 / \partial T$  of its dielectric constant  $\epsilon_2$ .

8. The voltage sensor as claimed in one of the preceding claims, characterized in that a stack of  $N$  elements of the electro-optically active medium (1) and  $N+1$  elements of the distance medium (2) is arranged between the electrodes (3, 4),  $N$  being an integer where  $N \geq 1$ , and an element of the electro-optically active medium (1) in each case being arranged between two adjacent elements of the distance medium (2), the first and the last element in the stack being in contact with a respective one of the two electrodes (3, 4) and, in particular, each of the elements being essentially

cylindrical with essentially the same cylinder diameter.

9. The voltage sensor as claimed in claim 8,  
5 characterized in that the elements of the electro-  
optically active medium (1) have such an effective  
thickness and are arranged between the electrodes (3,  
4) in such a way that a deviation between the voltage  
determined by means of the voltage sensor and the  
10 voltage V to be measured is minimal.

10. The voltage sensor as claimed in claim 8,  
characterized in that the elements of the electro-  
optically active medium (1) all have the same effective  
15 thickness  $\delta_1 = d_1/N$ , and in that either

(a) the elements of the distance medium (2) have an  
effective thickness  $\delta_2 = d_2/N$ , but the outer two  
elements of the distance medium (2) in the stack have  
an effective thickness  $\delta_2' = d_2/(2 \cdot N)$ , or in that  
20 (b) the elements of the distance medium (2) have an  
effective thickness  $\delta_2 = d_2/(N+1)$ .

11. The voltage sensor as claimed in one of the  
preceding claims, characterized in that the electrodes  
25 (3, 4) together with the electro-optically active  
medium (1) and the distance medium (2) are cast in  
silicone (15).

12. The voltage sensor as claimed in one of the  
30 preceding claims, characterized in that the electrodes  
(3, 4) together with the electro-optically active  
medium (1) and the distance medium (2) are cast in  
silicone, the silicone in the region of the electrodes  
(3, 4), of the electro-optically active medium (1) and  
35 of the distance medium (2) being formed essentially in  
cylindrical or barrel-shaped fashion with a diameter  
which is between 1.1 and 6 times, in particular between

2 and 4 times, as large as a maximum radial extent of the electrodes (3, 4).

13. The voltage sensor as claimed in claim 11 or 12,  
5 characterized in that the silicone (15) in the region of the electrodes (3, 4), of the electro-optically active medium (1) and of the distance medium (2), is formed essentially in cylindrical or barrel-shaped fashion, and the electrodes (3, 4) have electrically  
10 conductive voltage feeds (3b, 4b), which are formed essentially in rod-type fashion and are likewise cast in silicone, the silicone (15) in the region of the voltage feeds (3b, 4b) being formed essentially in cylindrical fashion and having a smaller diameter than  
15 in the region of the electrodes (3, 4), of the electro-optically active medium (1) and of the distance medium (2), and, in particular, in that the silicone has a shielding on the outside.

20 14. The voltage sensor as claimed in one of the preceding claims, characterized in that the electro-optically active medium (1) is crystalline BGO which is oriented with its [001] direction parallel to the direction of propagation of the light (5), in that the  
25 direction of propagation of the light (5) essentially runs along the electric field generated by the voltage V, and in that the distance medium (2) is fused silica.

15. A method for measurement of an electrical voltage  
30 V, the voltage V being present between two electrodes (3, 4) arranged in a manner spaced apart from one another and generating an electric field, light (5) being radiated into an electro-optically active medium (1) arranged between the electrodes (3, 4), a state of  
35 polarization of the light (5) being influenced in the electro-optically active medium (1) by means of the electric field and the light being detected after emergence from the electro-optically active medium (1)

and the voltage  $V$  being determined from the detected state of polarization, characterized in that

5 a distance medium (2) is arranged between the two electrodes (3, 4), an effective thickness  $d_2$  of the distance medium (2) and an effective thickness  $d_1$  of the electro-optically active medium (1) being chosen in such a way that temperature influences on the detected state of polarization of the light (5) are essentially

10 compensated for.